

The Gas Cooled Fast Reactor (GFR)

Richard Stainsby on behalf of the GFR SSC
National Nuclear Laboratory, UK (Euratom)

With contributions from:
Christian Poette (CEA)
Akos Horvath, MTA-EK, Hungary (Euratom)
Tatsuya Hinoki, Kyoto University, Japan

Motivation

- **Fast reactors are important for the sustainability of nuclear power:**
 - **More efficient use of fuel**
 - **Reduced volumes, heat loading and radiotoxicity of high level waste**
- **Sodium cooled fast reactors are the shortest route to FR deployment, but:**
 - **The sodium coolant has some undesirable features:**
 - » **Chemical incompatibility with air and water**
 - » **Difficult to carry out inspection and repair**
 - » **Avoiding sodium boiling places a restriction on achievable core outlet temperature**
- **Gas cooled fast reactors do not suffer from any of the above:**
 - **Chemically inert, very stable nucleus, void coefficient is small (but positive), single phase coolant eliminates boiling and optically transparent.**

Motivation

- ***But ...***
 - ***Gaseous coolants have little thermal inertia -> rapid heat-up of the core following loss of forced cooling;***
 - » ***Compounded by the lack of thermal inertia of the core structure (no moderator) + high power density***

Advantages and Disadvantages of GFR

Advantages:

- **Low (+ve) coolant void coefficient**
- **Operation at high or very high temperatures**
- **Strong Doppler effect**
- **Transparent coolant**
- **Nuclear stability of the coolant – no activation products**
- **Chemical stability – no dissociation and chemically inert**
- **Negligible corrosion/erosion of reactor structures**
- **Passive decay heat removal to an independent heat sink**

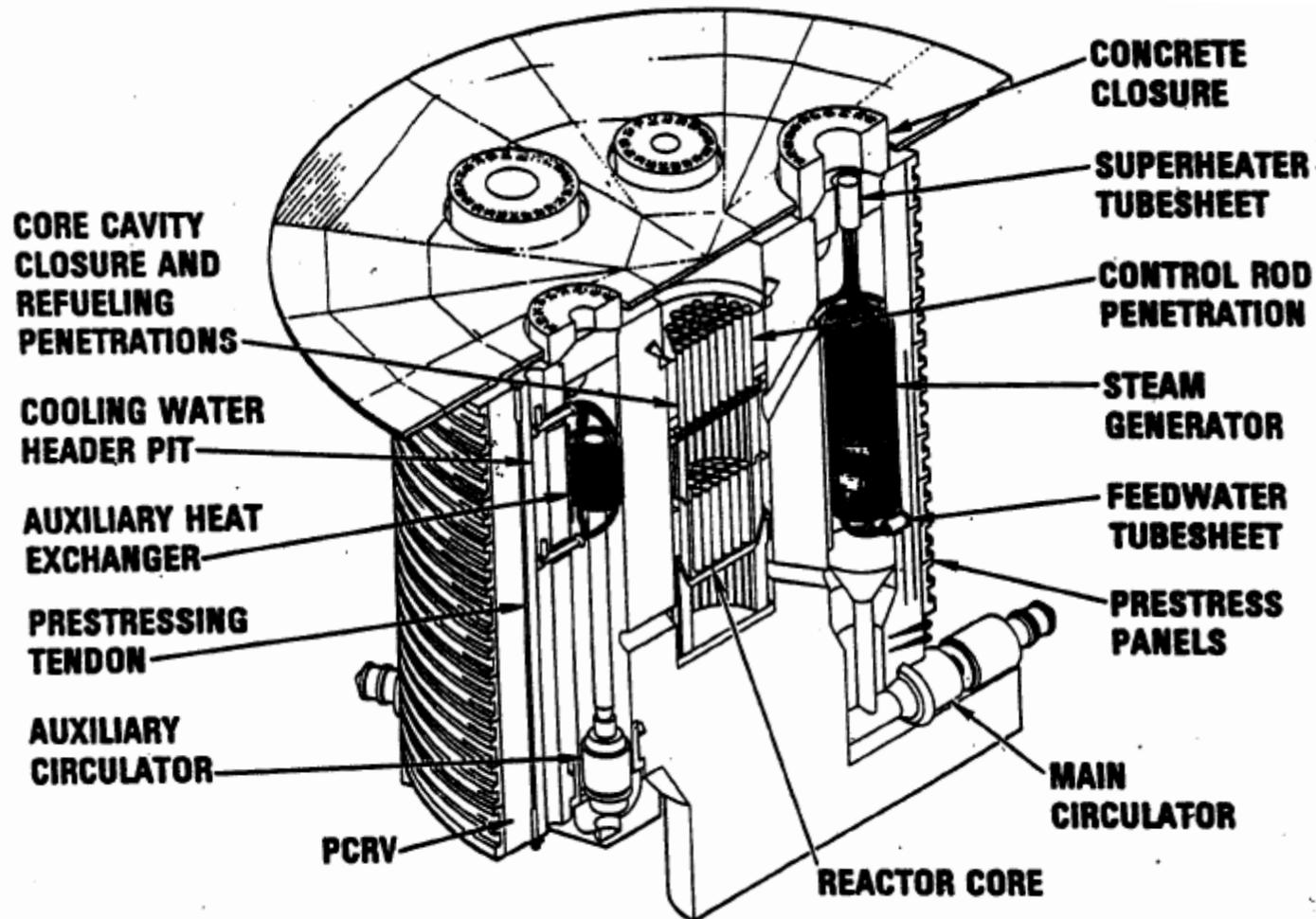
Disadvantages:

- **Pressurised system**
- **High coolant pumping power**
- **High power density, high temperature fuels are required**
- **Low thermal inertia gives short grace times, and ...**
- **It is difficult to remove decay heat by passive means in depressurised conditions**
 - **so multiple layers of engineered safety features are required**

Gas cooled fast reactor concepts: a partial historical perspective

- ***US, General Atomics – The GCFR programme***
 - ***Started in the 1960's***
 - ***Capitalised upon High Temperature (thermal) Reactor (HTR) experience:***
 - » ***Peach Bottom and Fort St Vrain***
 - ***Funded by US DOE***
 - ***Collaboration with European partners***
- ***Helium cooled reactor with a multi-cavity pre-stressed concrete pressure vessel. Featured a vented fuel pin fuel element design to reduce fuel clad stresses.***

General Atomics GCFR concept



Germany: the Gas Breeder Memorandum

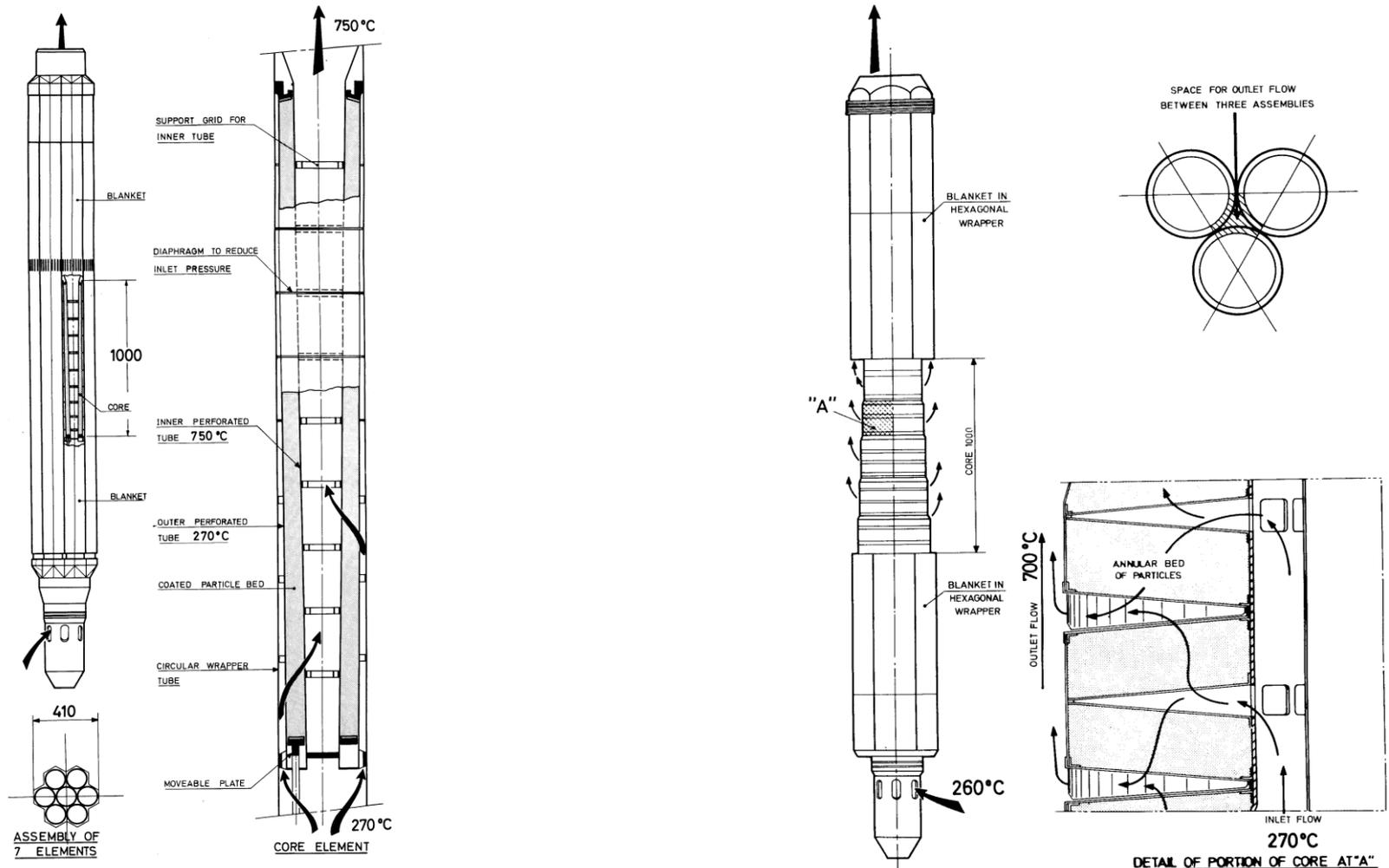
- ***Germany: the Gas Breeder Memorandum (1969)***
 - ***The German research centres at Karlsruhe and Jülich, together with industrial partners,***
 - ***Defined three concepts, all cooled by helium,***
 - ***Fuel assemblies extrapolated from sodium cooled fast reactors,***
 - ***Pre-stressed concrete pressure vessels***
 - ***Steam cycle,***
 - ***Some work was carried out on coated particle fuels and direct cycle power cycles.***

Europe: the Gas Breeder Reactor Association (1970 - 1981)

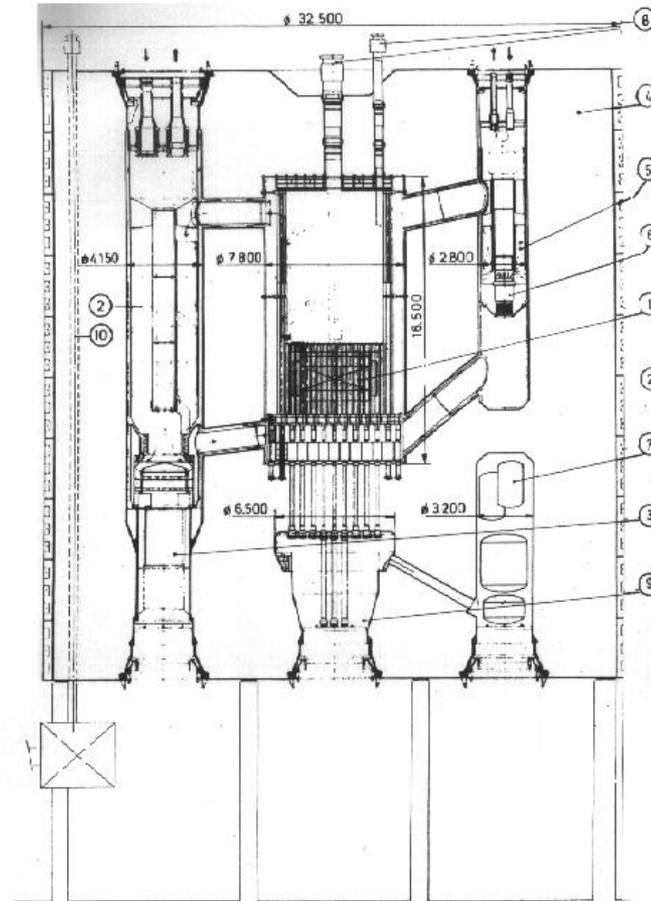
A number of organisations joined to form the Gas Breeder Reactor Association. Four designs were developed:

- GBR-1, a 1000MWe helium cooled reactor with metallic clad pin fuel***
- GBR-2, 1000MWe reactor using coated particle fuel, slightly elevated outlet temperature, helium coolant,***
- GBR-3 1000MWe reactor using coated particle fuel, CO₂ coolant***
- GBR-4 design was developed to avoid complexities of the particle bed fuel elements.***
 - Rib-roughened metal-clad fuel pins held in spacer grids.***

GBR-2 (left) and GBR-3 (right) particle bed fuel assemblies



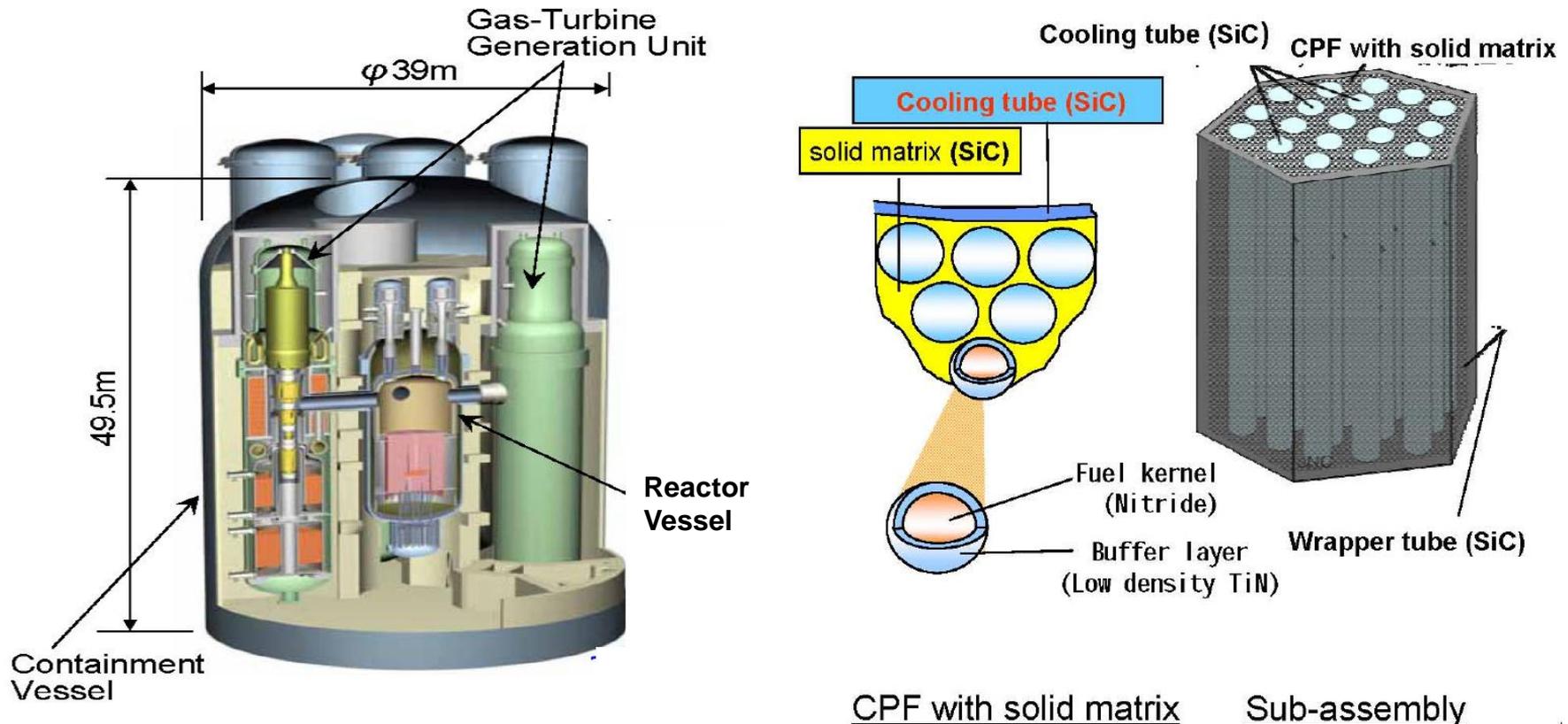
GBR-4 reactor layout



- 1 REACTOR CORE
- 2 MAIN STEAM GENERATOR
- 3 MAIN CIRCULATOR SET
- 4 PRESTRESSED CONCRETE VESSEL
- 5 EMERGENCY CONDENSER
- 6 EMERGENCY CIRCULATOR SET
- 7 FUEL VENTING PLANT AND H₂ PURIFICATION WELLS
- 8 REFUELLING STANDPIPES
- 9 LOWER CAVITY
- 10 SPENT FUEL TRANSFER TUBE

Japan: Coated Particle Fuels (1960s – present day)

- JAEA investigated both block fuel containing coated particles and packed bed (GBR-2 type) fuel elements.



The early GIF years – The exploratory phase

Participants US, France, Switzerland, Japan, UK & Euratom shared the analysis of six evaluation cases:

- ***Case 1 – 600 MWth, high temperature high power density, high density dispersed (plate) carbide fuel, direct cycle EC***
- ***Case 2 – As Case 1 but with a moderate temperature indirect S-CO₂ cycle EC***
- ***Case 3 – 2400 MWth, high temperature, high power density, moderate density dispersed carbide fuel (plate), direct cycle***
- ***Case 4 – As Case 3 with SiC-clad pin fuel (carbide)***
- ***Case 5 – 2400 Mth, high temperature, moderate power density, particle fuel (nitride), direct cycle energy conversion***
- ***Case 6 – 2400 MWth, high temperature, moderate power density, SiC-clad oxide fuel, direct cycle***

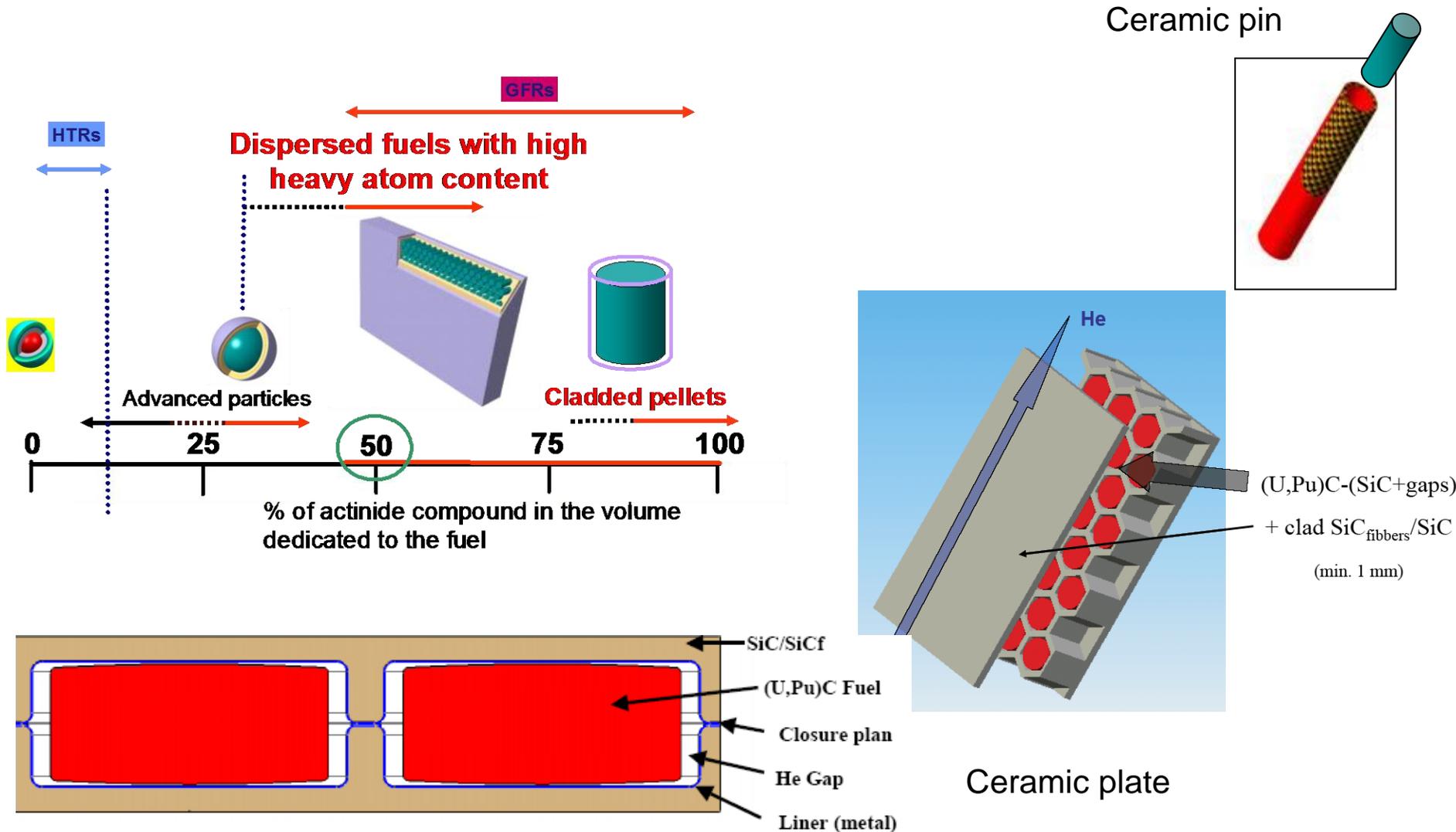
Core performance comparison

	Case 3 (carbide plate) (FR)	Case 4 (carbide pin) (US)	Case 5 (nitride, particle) (JP)	Case 6 (oxide, pin) (UK)
Fuel feasibility	?	?	?	? 
Fuel temp.				
Core pressure drop				
Pu inventory				
Breeding gain				
He void				

Outcome of exploratory phase down-selection

- ***600 MWth cores (Case 1 and Case 2) rejected on the basis of not meeting breeding ratio ≥ 1.0 (without breeding blankets)***
- ***At 2400 MWth, Case 5 (particle fuels) could not meet breeding gain objective without the use of breeder blankets***
- ***Case 3 was initially selected for study in the conceptual phase as the reference, but the direct cycle option was soon dropped in favour of an indirect helium-nitrogen Brayton / steam combined cycle.***
- ***CerCer plate fuel option was later dropped in favour of SiC-SiCf ceramic matrix composite pin***

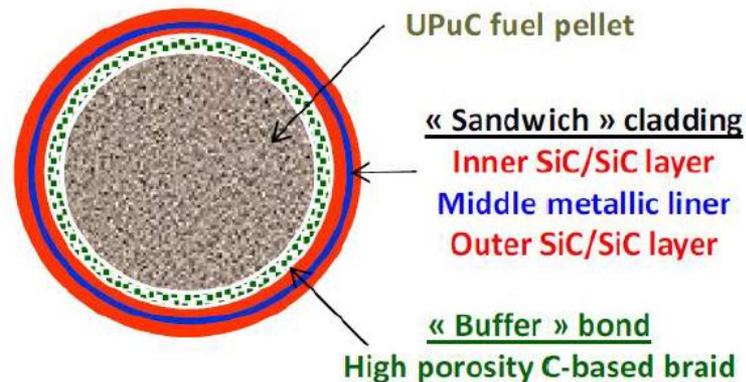
Potential GFR fuel forms



Current Fuel Pin Concept (CEA)

Although the plate type concept is attractive, fabrication difficulties appeared which lead to focus first on the more classical pin concept

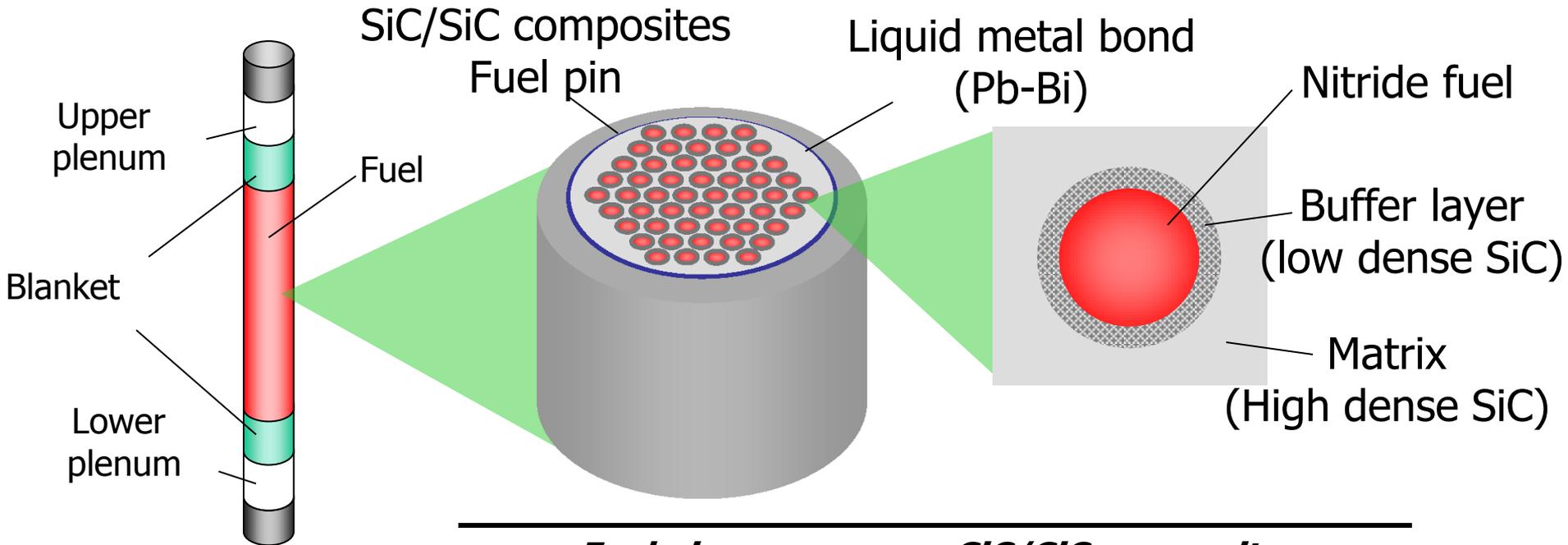
- a ceramic matrix composite cladding comprising a sandwich of SiC cladding and a thin internal metallic liner to ensure the leak tightness of the pin,
- a “buffer”, porous carbon structure placed between the pellet and the cladding allowing higher heat exchanges and moderate clad/pellet mechanical interaction.



The concept lives on as the basis for much current global work on Accident Tolerant Fuels (ATF) for light water reactors – **GFR's gift to the world !**

***... but work on coated particle fuels for
GFR continues here in Japan ...***

GFR Core Design Concept Using Fuel Pin



Fuel pin

SiC/SiC composites

Bond material

Liquid metal (Pb-Bi)

Fuel matrix

High dense SiC (> 95%TD)

Fuel buffer layer

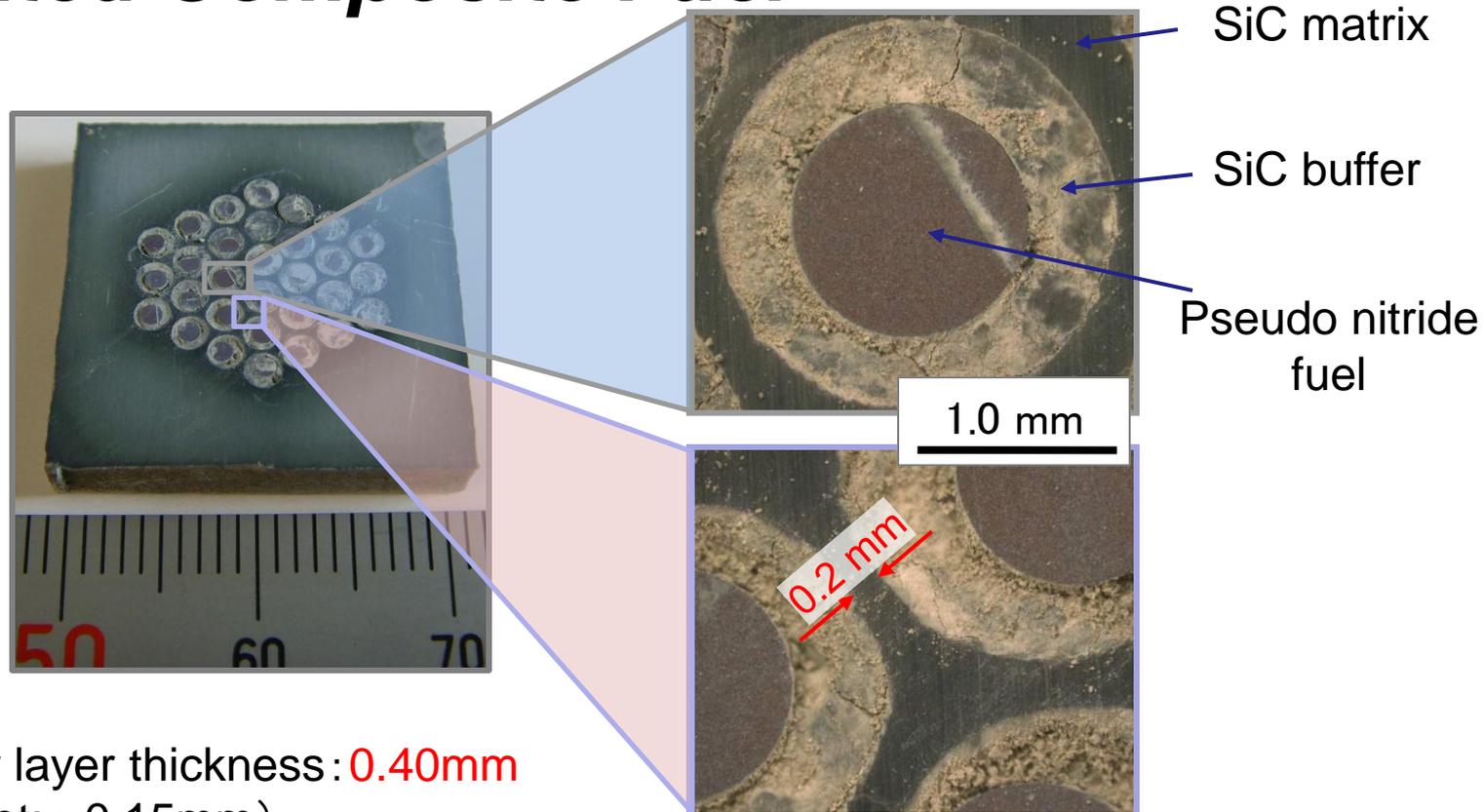
Low dense SiC (~ 50%TD)

Kyoto University

Fuel

Nitride fuel

Fabricated Composite Fuel



- ❑ Buffer layer thickness: **0.40mm**
(Target: >0.15mm)
- ❑ SiC matrix thickness: **0.22mm**
(Target: <0.23mm)
- ❑ Buffer layer density: **20%**
(Target: <50%)



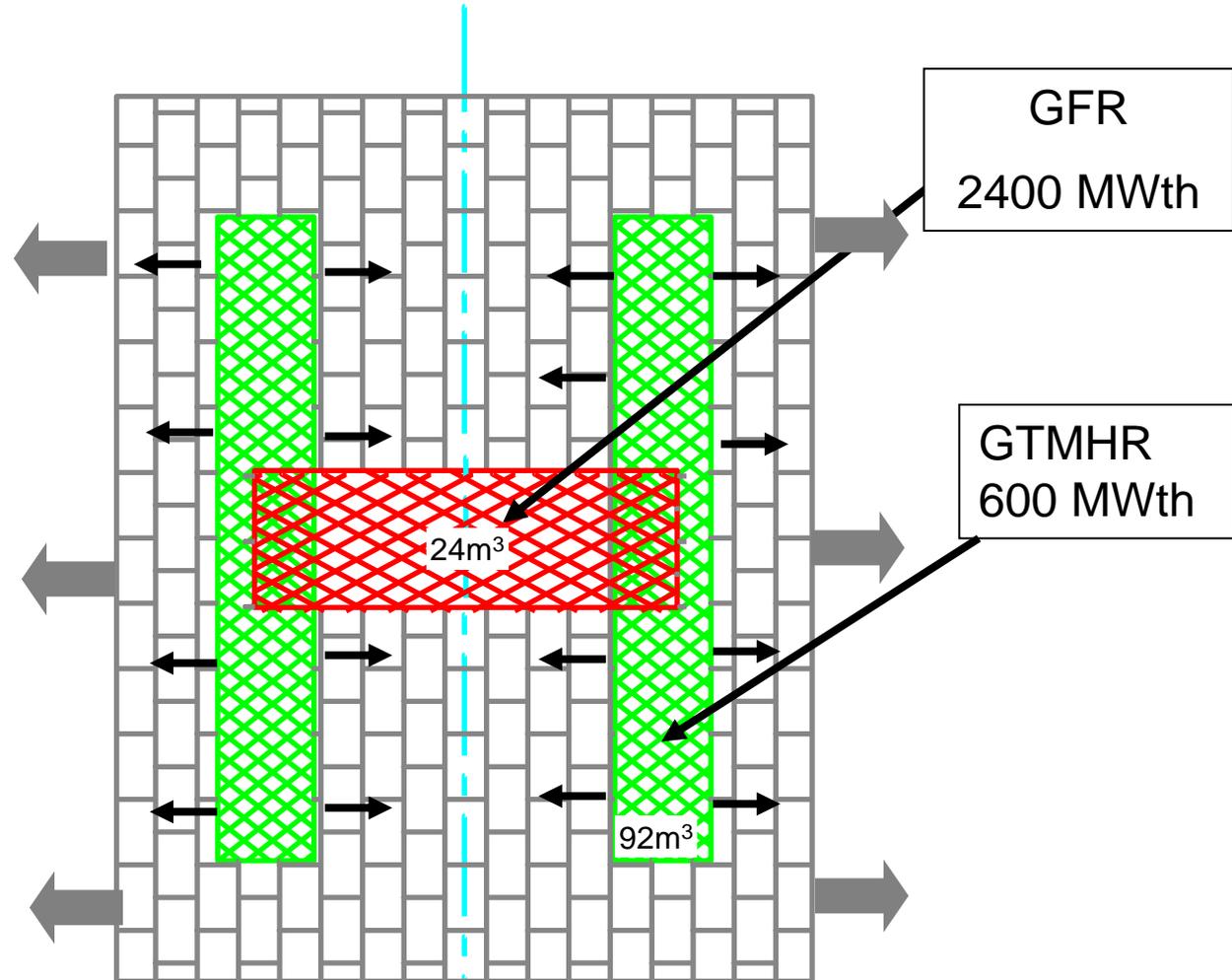
All technical targets were cleared with sufficient margin!

Kyoto University

GFR Fuel – the future (or possible futures)

- ***The “sandwich clad” fuel pin design appears to be viable***
- ***Work has been done on non-active thermal testing and irradiating the individual components.***
- ***Next steps are:***
 - ***To demonstrate end-cap sealing***
 - ***To produce rodlets***
 - ***To irradiate rodlets and to carry out PIE***
- ***It would be good if advantage could be taken from parallel work on accident tolerant fuels for light water reactors.***
- ***Coated particle fuels look like a good alternative but we would need to drop the proliferation resistance objective of having no breeder blankets***
 - ***Is it possible to retain PR objective with breeder blankets by spiking the these with minor actinides ?***

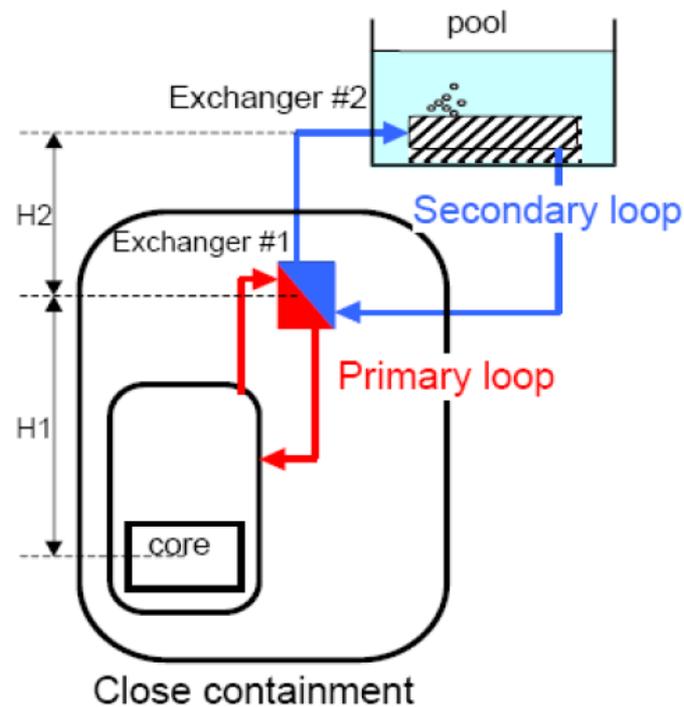
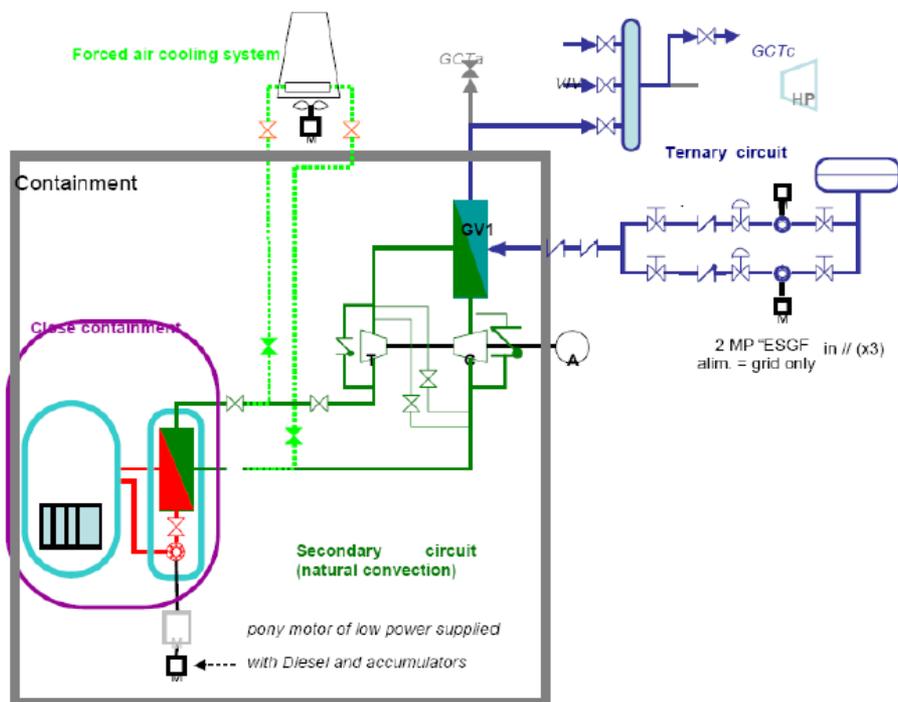
Comparison of passive heat conduction paths and power densities for GT-MHR and GFR2400 cores



GFR Safety Aspects

Decay heat removal relying on gas circulation in the Primary circuit

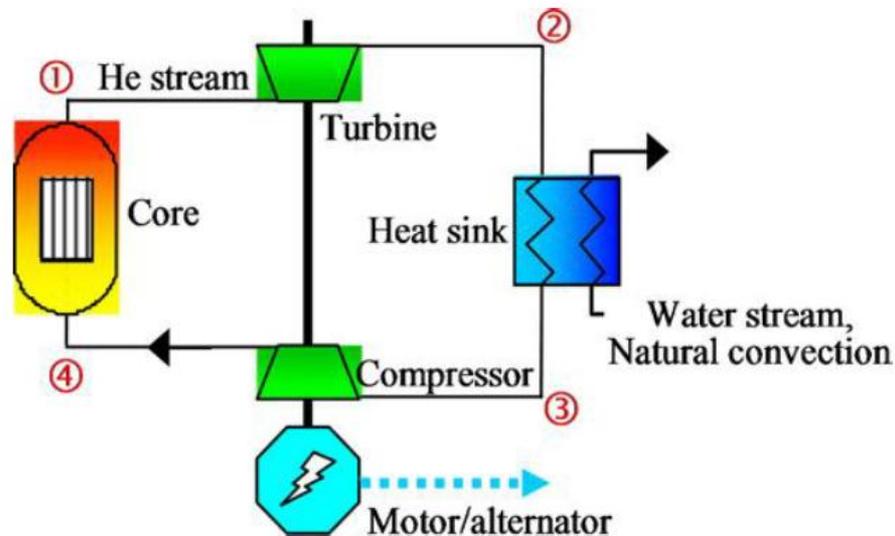
- Using at first normal circuits operated in forced or natural circulation
- Using dedicated DHR loops operated in forced or natural circulation



GFR Safety Enhancement

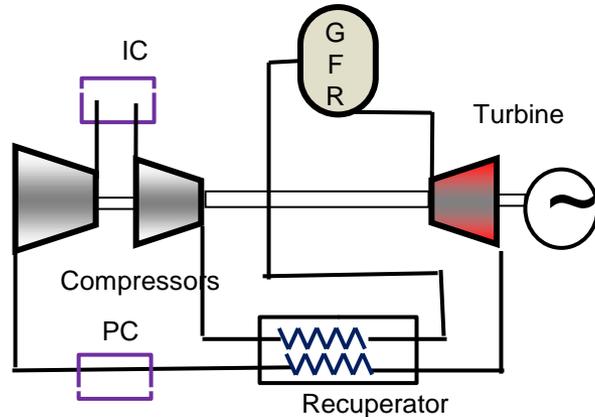
Still various open innovative design options

- **DHR system design:** the concept of autonomous Brayton cycle for DHR is promising; it should be incorporated in the existing DHR architecture as an extra protection line in the prevention of severe accidents.

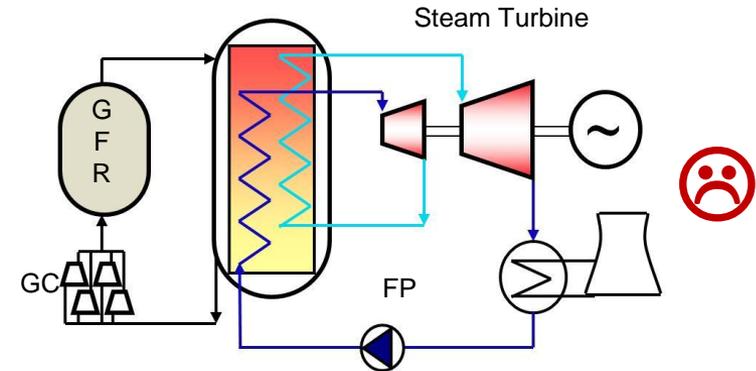


Principle scheme of the autonomous DHR loop: the primary gas circulation is ensured by a small turbo machine driven by the residual heat of the core

Power conversion system options



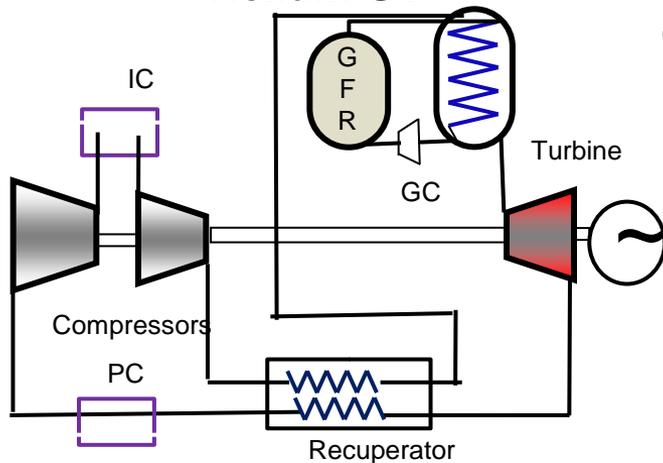
Direct Recuperated Helium GT



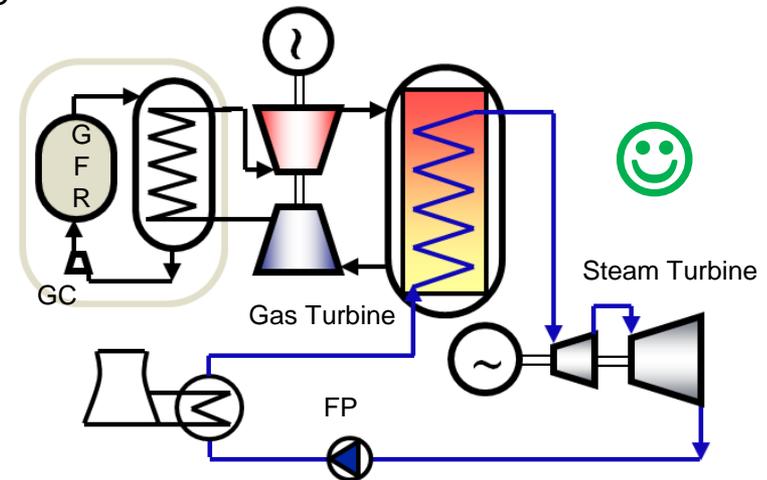
Indirect Pure Steam Cycle



PC – pre-cooler
 IC – Intercooler
 FP – Feed water pump
 GC – Gas circulators



Indirect Recuperated Helium GT

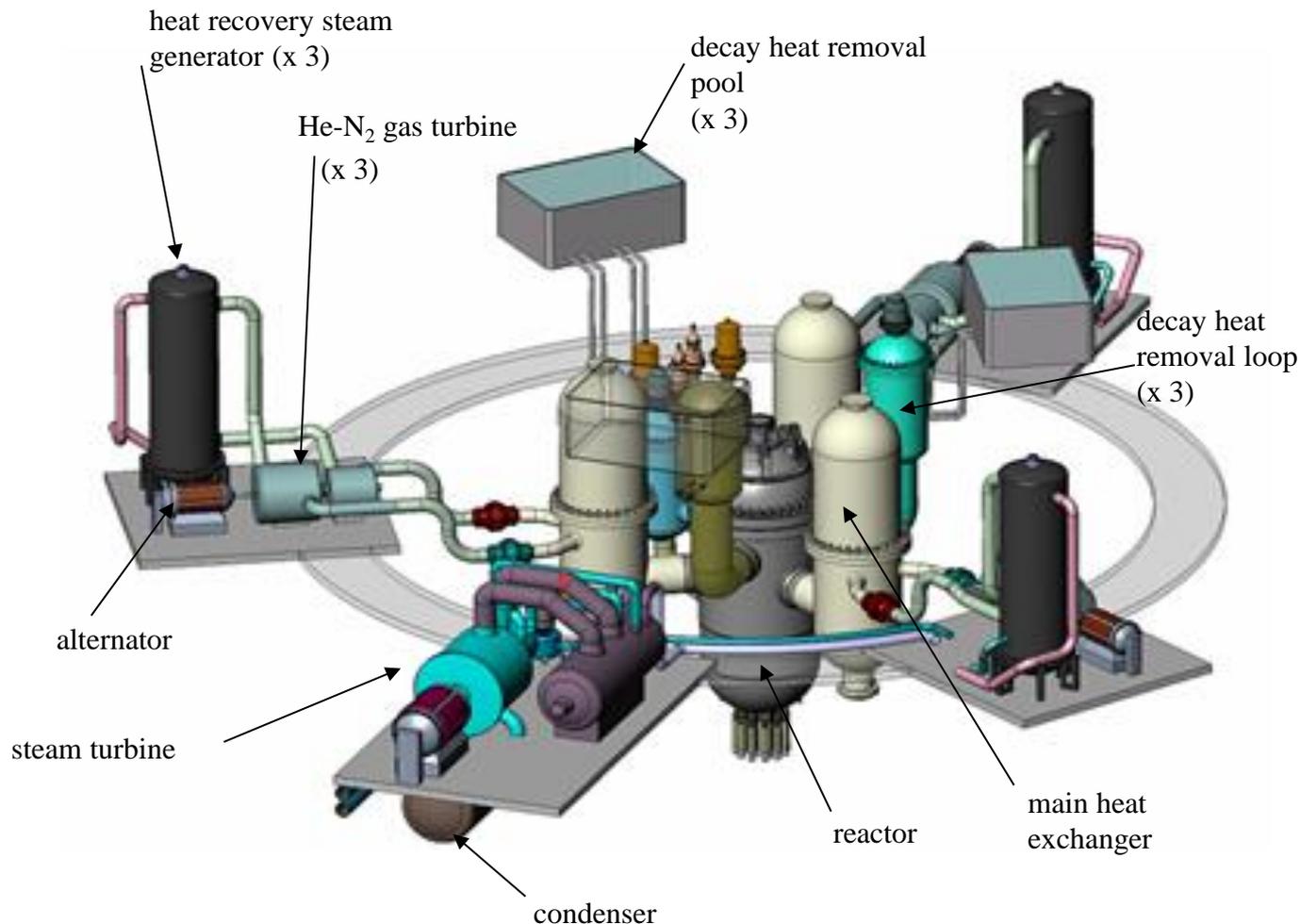


Indirect CCGT



Images courtesy of
 Chris Neeson, Rolls-Royce plc

Power conversion system (indirect combined gas~steam cycle)



Status of GFR System Cooperation

*GFR **System Arrangement** signed by Euratom, France, Switzerland and Japan*

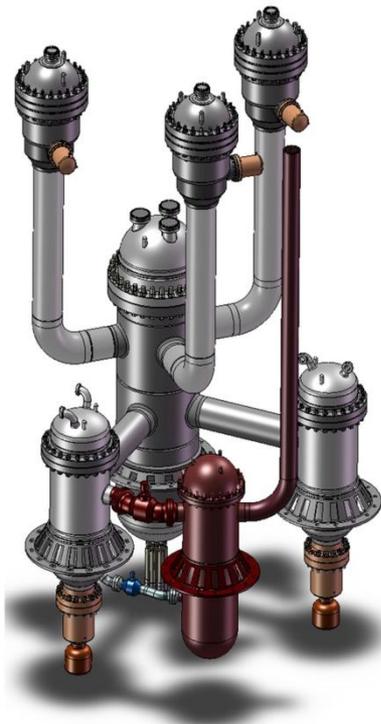
- *France – very limited effort which has been dedicated to supporting the V4 ALLEGRO consortium*
- *Switzerland – No national funding for GFR R&D*
- *Japan – No national funding for GFR R&D and efforts re-directed post-Fukushima, but Kyoto University is contributing to fuel development.*
- *Euratom: FP7 GoFastR project ended in February 2013:*
 - *Work surrounding establishment of ALLEGRO in the FP7 ALLIANCE project. Minor physics tasks in FP7 ESNII+,*
 - *There was a poor match between first call for in the Horizon 2020 programme and the needs of GFR*
 - » *Next Horizon 2020 call will be published at the end of 2015 for projects starting in 2017*

ALLEGRO – The GFR Demonstrator

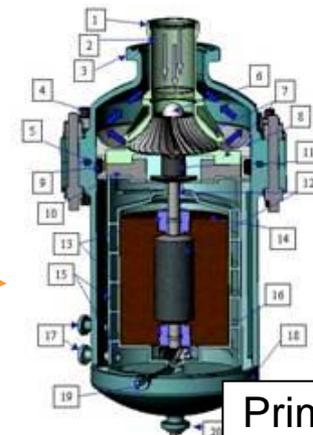
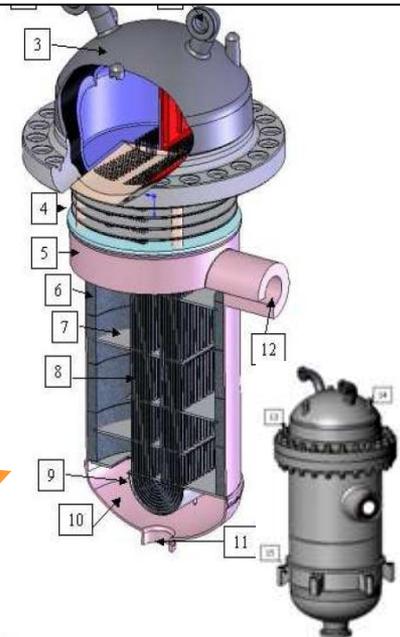
Main IHX, based on design of HTTR IHX by JAEA



GFR



Reactor vessel
Length : 14m
Diameter : 3.20 m



Primary Blower

The new ALLEGRO strategy - 1

A new strategy for developing the ALLEGRO reactor is under preparation, starting from April 2014. The main components of this strategy are as follows:

- To reduce ALLEGRO power from 75 MWth to around 10 MWth and to find the optimum core configuration;*
- To optimize nitrogen injection (launch time, duration) and the backup pressure in guard containment;*
- To increase main blowers inertia to avoid short term peak temperature for the LOCA+ blackout case and/or to develop a design with a gas turbine in the secondary side coupled to the primary blowers (this is the solution also advised for GFR).*

As a consequence of potential fuel supply difficulties it was also decided to use UO₂ pellets in AIM1 cladding instead of MOX pellets.



The new ALLEGRO strategy - 2

- *Ideas on high temperature remained unchanged.*
- *The design should ensure the possibility of increasing reactor power (eventually up to 75 MWth) if safety considerations allow for it.*
- *The initial core (UO₂ / AIM1) will be replaced by ceramic clad fuel whenever the development and qualification of this fuel will have been completed.*
- *A new system Roadmap is under preparation to cover all design, safety and experimental aspects of ALLEGRO development.*

Conclusions

- *The GFR concept is not new, having been explored by a number of countries since the 1960's*
- *GFR can be considered as a longer term fast reactor concept that will provide an equivalent of VHTR that can sustain a self-sustaining closed fuel cycle.*
- *Progress in the early days of the GIF was good with six partners all contributing to the exploratory phase.*
- *Formal signing of the system arrangement reduced the number of partners to four, and effort has continued to decrease to to a shifting of priorities back to SFR, and a refocusing of R&D funding following the Fukushima accident.*
- *Viable concepts for fuel and cladding have been developed.*
- *Work remains to be done on refining the safety architecture such that the safety goals can be met in a cost effective manner.*

Conclusions (2)

- *Work continues in the V4G4 consortium on developing ALLEGRO to be a GFR demonstrator – funded at a fairly low level by the European Commission and the Governments of the V4 member states.*
- *ALLEGRO concept has been re-worked to start with a much smaller core 10MWth c.f. 75MWth, starting with UO₂ fuel as opposed to MOX*
- *There are synergies with the VHTR system that can be exploited if the GFR partners can get funding to collaborate, such as:*
 - *Pressure boundary materials and design,*
 - *Main heat exchangers and power conversion*
 - *Oil-free gas circulators and other helium circuit components.*
- *The future of the GFR system itself depends upon the will of the signatories to continue – whether this will remain will be demonstrated in 2016 when the current System Arrangement expires.*

Acknowledgements

I would like to acknowledge the support of the members of the GFR Sytem Steering Committee and CDS & FCM PMBs both present and past:

- **Present SSC members**
 - ***Konstantin Mikityuk (PSI), Alfredo Vasile (CEA), Koji Sato (JAEA), Akos Horvath (MTA_EK), Henri Paillere (Secretariat)***
- **GFR SSC - EG Liaison: Frank Carre**
- **Past SSC Chairs:**
 - ***Kevan Weaver (INL), Jaques Roualt (CEA), Pascal Anzieu (CEA)***
- **And many more ...**
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- ***Apologies to all I have forgotten to mention and to those whose names for whom have forgotten the spelling !***